#### 5.1.11.4 WAC FM NONLINEAR RESPONSE TERMS

As reported in Reference 5.1.11.4-1

Reference 5.1.11.4-1 - IOM 388-PAG-CCA98-14, "WAC FM Calibration Results: Nonlinear Response Terms", Bob West and Charlie Avis, July 20, 1998

### 5.1.11.4.1 INTRODUCTION

Linearity tests made during thermal vac calibration revealed a nonlinear behavior (see Section 5.1.11.2). Departures from linearity (decreased sensitivity at high DN levels) were strongest for gain 0 with 4X4 summing. This behavior was thought to be caused by losses in the summing well on the CCD chip. There may also be some contribution to nonlinearity from the A/D converter at high signal levels. Both of these scenarios would imply that nonlinear behavior would be the same for all pixels, a function only of the charge in the summation well, but would differ for each gain state. They also imply that a nonlinearity correction can be made to the DN to compensate for nonlinear behavior. In this report we derive interpolation tables for each gain state to correct for nonlinear effects.

#### 5.1.11.4.2 METHOD

Sequences of increasing exposures were used which were taken at temperatures of  $+25^{\circ}$  C (1x1) and  $+5^{\circ}$  C (2x2 and 4x4) using clear filters in both wheels. Gain 0 and 1 were taken in 4x4 and 2x2 mode respectively and Gain 2 and 3 in 1x1 mode. All data were taken with Antiblooming 'OFF'.

Multiple input files (usually 3) were combined at each exposure level to suppress data errors and improve the signal-to-noise ratio. In addition, bias and dark current values were subtracted from each of the 13-14 images in each exposure sequence.

The mean DN value for the central 100 by 100 region was tabulated. The IDL routine POLYFITW was used to find a best-fit value for the weighted dependent variable array DN/(exposure time) as a function of the independent variable exposure time. The first term in the derived coefficients gives the best-fit linear term (A). A correction factor is then tabulated as

$$C = At / DN(t)$$

where t is the exposure time and

DN(t) is the tabulated mean DN for that exposure time.

The problem is somewhat subtle because the lowest DN values should behave linearly but also have the greatest uncertainty because they are most sensitive to errors in dark subtraction. The

slopes derived from the POLYFITW routine are sensitive to the weighting functions. After several tries, a weighting scheme was settled on which favors the low DN part of the array but gives zero weight to the shortest non-zero exposure. The shortest non-zero exposures consistently produce higher DN values than would be expected from the fits to longer exposures. They are high by up to 16.1%. The linear fits are shown as straight lines in the plots that follow, and the observed DN values are plotted as + symbols.

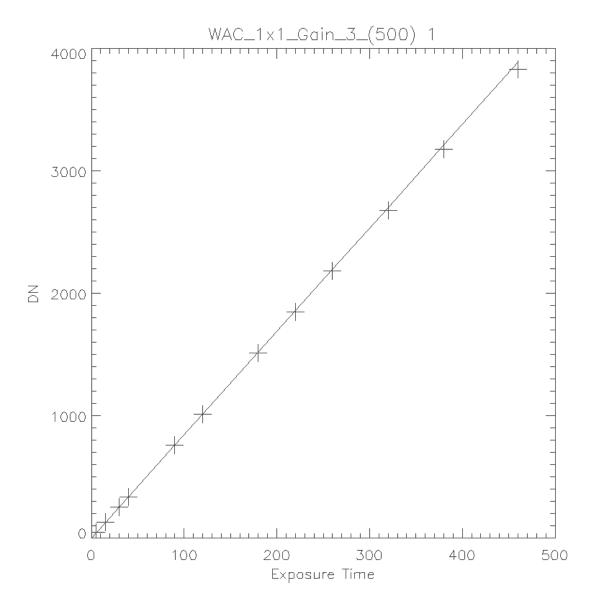


Figure 5.1.11.4-1 - Linear component of the fitted data (+) is plotted as the solid line. Summation is indicated in the title. Gain state is 3.

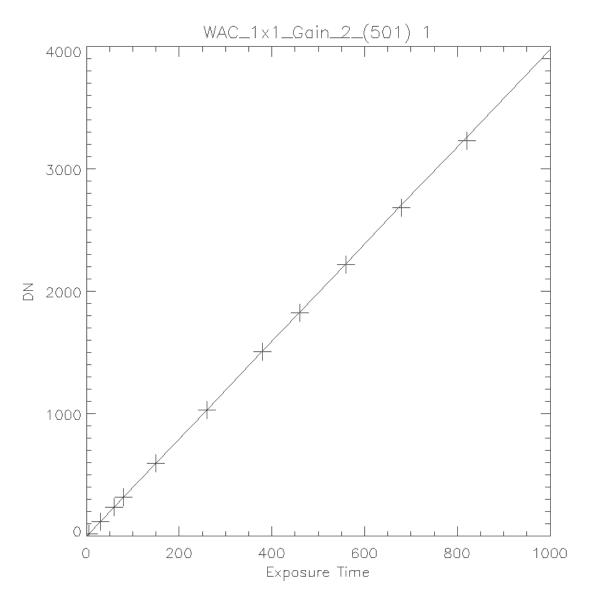


Figure 5.1.11.4-2 - Linear component of the fitted data (+) is plotted as the solid line. Summation is indicated in the title. Gain state is 2.

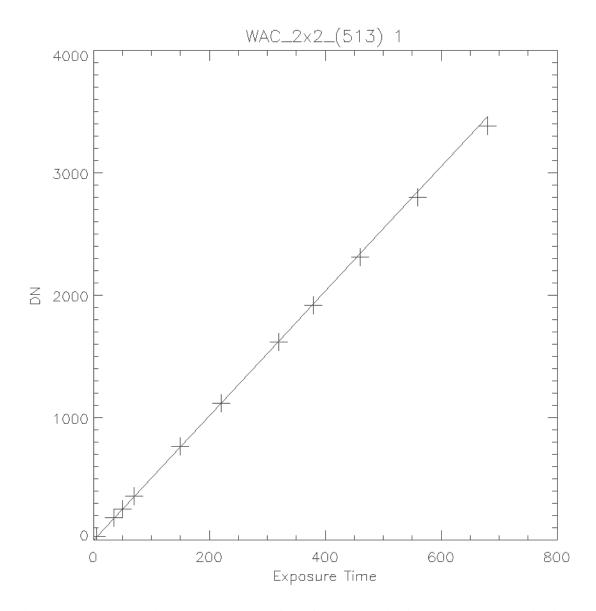


Figure 5.1.11.4-3 - Linear component of the fitted data (+) is plotted as the solid line. Summation is indicated in the title. Gain state is 1.

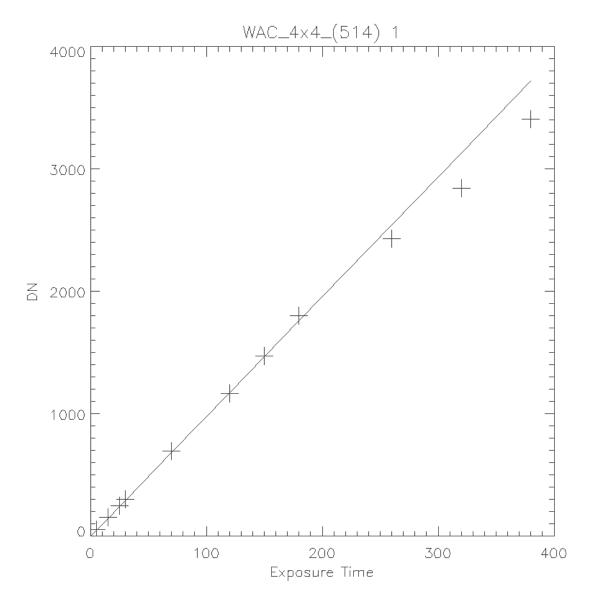


Figure 5.1.11.4-4 - Linear component of the fitted data (+) is plotted as the solid line. Summation is indicated in the title. Gain state is 0.

## 5.1.11.4.3 RESULTS

The correction factors tabulated below correct for nonlinearity by

DN' = DN\*C

where C is the correction factor,

DN is the observed DN (after dark-count and bias subtraction), and

DN' is the desired DN.

A correction algorithm can interpolate to get C as a function of observed DN for each pixel. This procedure should occur after the uneven bit weighting correction during the radiometric correction of each image. Note that DN' values greater than 4095 will result in some cases even though the data were not actually saturated. This fact will have an effect on the design of the radiometric correction software.

Correction factors for the four gain states are listed in the following table.

Gain 0		Gain 1		Gai	in 2	Gain 3		
DN	C	DN	C	DN	C	DN	C	
55.3	0.885	30.3	0.839	21.8	0.915	47.2	0.895	
153.5	0.957	182.4	0.977	121.2	0.985	131.4	0.965	
250.7	0.976	257.6	0.988	240.3	0.994	256.5	0.989	
300.5	0.977	359.6	0.991	320.1	0.995	340.8	0.992	
694.9	0.986	765.0	0.998	598.8	0.997	760.7	1.000	
1167.7	1.006	1118.5	1.001	1034.9	1.000	1012.1	1.002	
1472.7	0.997	1619.2	1.006	1509.9	1.002	1514.2	1.005	
1805.8	0.976	1917.9	1.009	1827.8	1.002	1848.6	1.006	
2430.6	1.047	2312.8	1.012	2219.6	1.004	2183.0	1.007	
2844.5	1.101	2803.6	1.017	2687.7	1.007	2681.0	1.009	
3405.9	1.092	3384.3	1.023	3231.7	1.010	3177.4	1.011	
4096.0	1.168	4096.0	1.029	3902.4	1.020	3830.6	1.015	
				4096.0	1.020	4096.0	1.016	

# 5.1.11.4.4 IMAGES USED IN NON-LINEARITY ANALYSIS

image day eventtime	observation	gain mo	de exp	image	day	eventtime	observation	gain	mode exp
+25°C 126930 180 4:43:13.0 126931 180 4:44:42.0 126932 180 4:46:11.0 126933 180 4:47:40.0	LTC_BLEM_GAIN_500 LTC_BLEM_GAIN_500 LTC_BLEM_GAIN_500 LTC_BLEM_GAIN_500	3 (40K) FUL 3 (40K) FUL 3 (40K) FUL 3 (40K) FUL	L 0 L 0 L 0 L 5	126874 126880 126881 126882	180 180 180 180	2:5:39.0 2:17:24.0 2:18:53.0 2:20:22.0	LTC_BLEM_GAIN_501 LTC_BLEM_GAIN_501 LTC_BLEM_GAIN_501 LTC_BLEM_GAIN_501	2 (100K) 2 (100K) 2 (100K) 2 (100K)	FULL 1000 FULL 1000 FULL 1000 FULL 1000
126932 180 446-140.0 126934 180 447-10.0 126934 180 447-10.0 126935 180 453-130.0 126936 180 453-130.0 126936 180 453-130.0 126937 180 453-130.0 126938 180 456-110.0 126940 180 455-140.0 126940 180 455-140.0 126942 180 5-145-0 126943 180 5-145-0 126944 180 5-145-0 126944 180 5-145-0 126944 180 5-145-0 126945 180 5-145-0 126946 180 5-14-0 126947 180 5-14-0 126948 180 5-16-10 126949 180 5-10-15 126949 180 5-10-15 126949 180 5-10-15 126949 180 5-10-15 126949 180 5-10-15 126949 180 5-10-15 126959 180 5-14-0 126959 180 1-14-3 126959	DESERVATION  LTC. BLEM_GAIN_500 LTC. BLEM_GAIN_501	3 (400K) FULL 2 (100K) FULL 2	L 0 5 5 5 1 L 15 5 5 L 15 5 L	126882 +5°C 130191 130191 130192 130193 130194 130193 130194 130193 130194 130201 1302	180 1955 1956 1	2:20:22.0  10:38:4.0 10:39:8.0 10:39:8.0 10:40:13.0 10:41:17.0 10:42:12.1 10:43:25.0 10:42:21.0 10:43:25.0 10:45:7.0	LTC BLEM GAIN 501 LTC BLEM GAIN 501 LTC BLEM GAIN 513 LTC BLEM GAIN 514 LTC BLEM GAI	2 (100K)  1 (400K)	SUM2 0 SUM2 0 SUM2 0 SUM2 0 SUM2 0 SUM2 5 SUM2 5 SUM2 35 SUM2 35 SUM2 50 SUM2 50 SUM2 50 SUM2 50 SUM2 50 SUM2 50 SUM2 150 SUM2 320 SUM2 380 SUM2 320 SUM2 320 SUM2 320 SUM2 320 SUM2 320 SUM2 320 SUM2 380 SUM2 380 SUM2 380 SUM2 560 SUM4 56
12069 100 1.58:37.0 126871 180 2:1:35.0 126879 180 2:16:18.0 126872 180 2:2:41.0 126873 180 2:4:10.0	LTC_BLEM_GAIN_501 LTC_BLEM_GAIN_501 LTC_BLEM_GAIN_501 LTC_BLEM_GAIN_501 LTC_BLEM_GAIN_501	2 (100K) FUI 2 (100K) FUI 2 (100K) FUI 2 (100K) FUI 2 (100K) FUI	LL 820 LL 820 LL 820 LL 1000 LL 1000	130262 130263 130264 130265	195 195 195 195 195	12:51:31.0 12:52:23.0 12:53:14.0 12:54:5.0	) LTC_BLEM_GAIN_514 ) LTC_BLEM_GAIN_514 ) LTC_BLEM_GAIN_514 ) LTC_BLEM_GAIN_514 LTC_BLEM_GAIN_514	0 (1400K 0 (1400K 0 (1400K 0 (1400K)	SUM4 320 SUM4 320 SUM4 380 SUM4 380 SUM4 380